

Numerical implementation of Manzari-Dafalias model in \mathbb{R}^3 and \mathbb{R}^6 space, a computational comparison

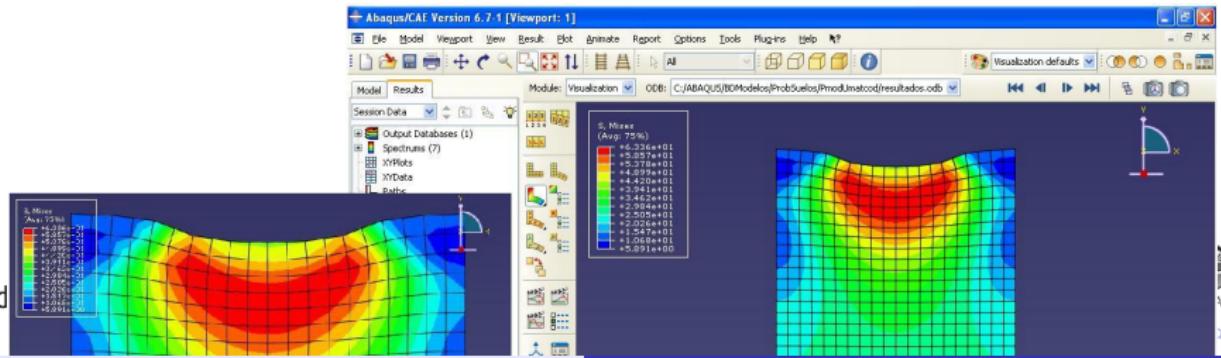
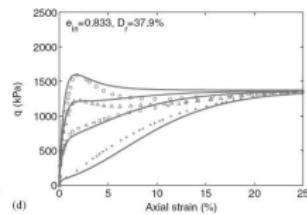
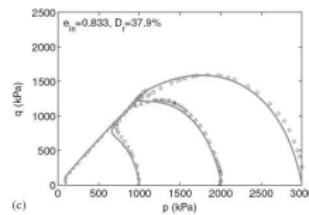
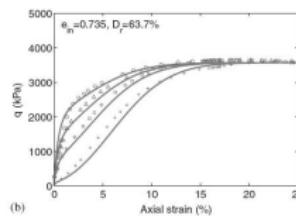
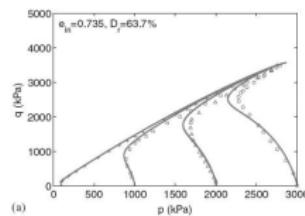
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Motivation

Toyura Sand - Dafalias (Sanisand, 2007), and New building in Civil Eng. Faculty, Univ. of the Cauca



- 1 Introduction and Basic Concepts
- 2 The model in multi-space
- 3 About of the numerical implementation
- 4 Model Constants, Nevada Sand (Arulmoni et. al., 1992)
- 5 Results and Discussion
- 6 Conclude Remarks

The model, Triaxial Space and plasticity

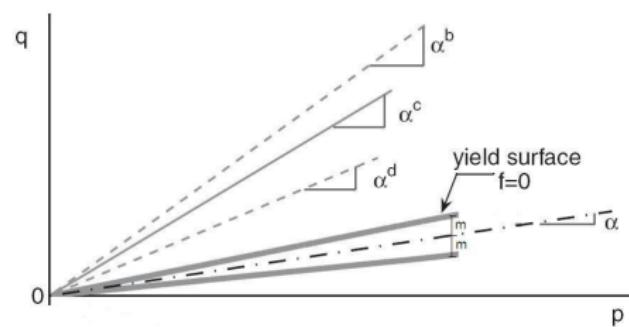
The Yield Surface

Yield surface in space p-q, Lawrence(1972)

$$f = \eta - \alpha \pm m = 0, f = q - p\alpha \pm mp = 0$$

α : Slope in $q - p$ space of the bisector of the ysurf.

$2m$: wedge 'opening' of the yield surf (angle). ($m = 0,05$)



The models developed over Elastic, hypoelastic and plastic theory,
Critical state soil mechanics and Bounding surface plasticity

Elastic and hypoelastic relations

The Yield Surface in multi-space

Is adopte

$$\dot{\varepsilon}_v^e = \frac{\dot{p}}{K} \quad (1)$$

$$\dot{\epsilon}^e = \frac{\dot{s}}{2G} \quad (2)$$

$$K = K_0 \left(\frac{p}{p_{atm}} \right)^a \quad (3)$$

$$G = G_0 \left(\frac{p}{p_{atm}} \right)^a \quad (4)$$

where $K_0, G_0, a (a \circlearrowleft 0,5)$: model parameter

p_{atm} : Atmospheric pressure

Yield surface

$$f = [(\mathbf{s} - p\boldsymbol{\alpha}) : (\mathbf{s} - p\boldsymbol{\alpha})]^{1/2} - \sqrt{\frac{2}{3}}mp = 0$$

$$f = [(\mathbf{r} - \boldsymbol{\alpha}) : (\mathbf{r} - \boldsymbol{\alpha})]^{1/2} - \sqrt{\frac{2}{3}}m = 0$$



back-stress ratio deviatoric tensor, $\mathbf{r} = \frac{\mathbf{s}}{p}$



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The model in multi-space and plasticity

Loading direction

Since consistency condition ($\dot{f} = 0$),
then:

$$\frac{\partial f}{\partial \sigma} = \mathbf{L} = \mathbf{n} - \frac{1}{3}N\mathbf{I} \quad (5)$$

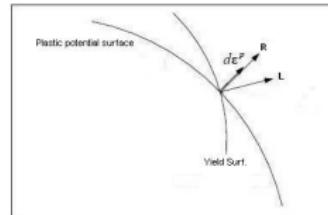
where:

$$\mathbf{n} = \frac{\mathbf{r} - \boldsymbol{\alpha}}{\sqrt{\frac{2}{3}m}} \quad (6)$$

$$N = \boldsymbol{\alpha} : \mathbf{n} + \sqrt{\frac{2}{3}m} \quad (7)$$

and:

L: Loading direction



$$\frac{\partial g}{\partial \sigma} = \mathbf{R} = \mathbf{n} - \frac{1}{3}D\mathbf{I} \quad (8)$$

Flow rule

$$\dot{\epsilon}^p = \langle L \rangle \mathbf{R} \quad (9)$$

where, D: Dilatancy coefficient, L:
Loading index

The strain tensor in covariant base in \mathbb{R}^6

$$[\bar{\varepsilon}_a] = \begin{bmatrix} \bar{\varepsilon}_1 \\ \bar{\varepsilon}_2 \\ \bar{\varepsilon}_3 \\ \bar{\varepsilon}_4 \\ \bar{\varepsilon}_5 \\ \bar{\varepsilon}_6 \end{bmatrix}^T = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ (\varepsilon_{12} + \varepsilon_{21}) \\ (\varepsilon_{23} + \varepsilon_{32}) \\ (\varepsilon_{31} + \varepsilon_{13}) \end{bmatrix}^T = \begin{bmatrix} \varepsilon_{11} \\ \varepsilon_{22} \\ \varepsilon_{33} \\ 2\varepsilon_{12} \\ 2\varepsilon_{23} \\ 2\varepsilon_{31} \end{bmatrix}^T \quad (10)$$

$$\begin{aligned} \mathbf{G}_1 &= \hat{\mathbf{e}}_1 \otimes \hat{\mathbf{e}}_1, & \mathbf{G}_4 &= \hat{\mathbf{e}}_1 \otimes \hat{\mathbf{e}}_2 + \hat{\mathbf{e}}_2 \otimes \hat{\mathbf{e}}_1 = 2\hat{\mathbf{e}}_1 \otimes \hat{\mathbf{e}}_2, \\ \mathbf{G}_2 &= \hat{\mathbf{e}}_2 \otimes \hat{\mathbf{e}}_2, & \mathbf{G}_5 &= \hat{\mathbf{e}}_2 \otimes \hat{\mathbf{e}}_3 + \hat{\mathbf{e}}_3 \otimes \hat{\mathbf{e}}_2 = 2\hat{\mathbf{e}}_1 \otimes \hat{\mathbf{e}}_2, \\ \mathbf{G}_3 &= \hat{\mathbf{e}}_3 \otimes \hat{\mathbf{e}}_3, & \mathbf{G}_6 &= \hat{\mathbf{e}}_3 \otimes \hat{\mathbf{e}}_1 + \hat{\mathbf{e}}_1 \otimes \hat{\mathbf{e}}_3 = 2\hat{\mathbf{e}}_1 \otimes \hat{\mathbf{e}}_2 \end{aligned} \quad (11)$$

$$[G_{ab}] = [G_a : G_b] = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 2 \end{bmatrix} \quad (12)$$

The stress tensor in contravariant base in \mathbb{R}^6

$$[G^{ab}] = [G_{ab}]^{-1} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1/2 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1/2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1/2 \end{bmatrix} \quad (13)$$

$$\begin{aligned} \mathbf{G}^1 &= \hat{\mathbf{e}}^1 \otimes \hat{\mathbf{e}}^1, & \mathbf{G}^4 &= \frac{1}{2}(\hat{\mathbf{e}}^1 \otimes \hat{\mathbf{e}}^2 + \hat{\mathbf{e}}^2 \otimes \hat{\mathbf{e}}^1) = \hat{\mathbf{e}}^1 \otimes \hat{\mathbf{e}}^2, \\ \mathbf{G}^2 &= \hat{\mathbf{e}}^2 \otimes \hat{\mathbf{e}}^2, & \mathbf{G}^5 &= \frac{1}{2}(\hat{\mathbf{e}}^2 \otimes \hat{\mathbf{e}}^3 + \hat{\mathbf{e}}^3 \otimes \hat{\mathbf{e}}^2) = \hat{\mathbf{e}}^2 \otimes \hat{\mathbf{e}}^3, \\ \mathbf{G}^3 &= \hat{\mathbf{e}}^3 \otimes \hat{\mathbf{e}}^3, & \mathbf{G}^6 &= \frac{1}{2}(\hat{\mathbf{e}}^3 \otimes \hat{\mathbf{e}}^1 + \hat{\mathbf{e}}^1 \otimes \hat{\mathbf{e}}^3) = \hat{\mathbf{e}}^1 \otimes \hat{\mathbf{e}}^3 \end{aligned} \quad (14)$$

$$[\bar{\sigma}^a] = \begin{bmatrix} \bar{\sigma}^1 \\ \bar{\sigma}^2 \\ \bar{\sigma}^3 \\ \bar{\sigma}^4 \\ \bar{\sigma}^5 \\ \bar{\sigma}^6 \end{bmatrix} = \begin{bmatrix} \sigma^{11} \\ \sigma^{22} \\ \sigma^{33} \\ 1/2(\sigma^{12} + \sigma^{21}) \\ 1/2(\sigma^{23} + \sigma^{32}) \\ 1/2(\sigma^{31} + \sigma^{13}) \end{bmatrix} = \begin{bmatrix} \sigma^{11} \\ \sigma^{22} \\ \sigma^{33} \\ \sigma^{12} \\ \sigma^{23} \\ \sigma^{31} \end{bmatrix} \quad (15)$$

Elastic Tensor

For each index $a = \{1, 2, 3, 4, 5, 6\}$ exist a pair $\{i, j\} = \{\{1, 1\}, \{2, 2\}, \{3, 3\}, \{1, 2\}, \{2, 3\}, \{3, 1\}\}$. The same manner for index b with the kl .

$$[\bar{D}^{ab}] = \begin{bmatrix} \bar{D}^{11} & \bar{D}^{12} & \bar{D}^{13} & \bar{D}^{14} & \bar{D}^{15} & \bar{D}^{16} \\ \bar{D}^{21} & \bar{D}^{22} & \bar{D}^{23} & \bar{D}^{24} & \bar{D}^{25} & \bar{D}^{26} \\ \bar{D}^{31} & \bar{D}^{32} & \bar{D}^{33} & \bar{D}^{34} & \bar{D}^{35} & \bar{D}^{36} \\ \bar{D}^{41} & \bar{D}^{42} & \bar{D}^{43} & \bar{D}^{44} & \bar{D}^{45} & \bar{D}^{46} \\ \bar{D}^{51} & \bar{D}^{52} & \bar{D}^{53} & \bar{D}^{54} & \bar{D}^{55} & \bar{D}^{56} \\ \bar{D}^{61} & \bar{D}^{62} & \bar{D}^{63} & \bar{D}^{64} & \bar{D}^{65} & \bar{D}^{66} \end{bmatrix} \quad (16)$$

rewritten the index of \mathbb{R}^3 :

$$[\bar{D}^{ab}] = \begin{bmatrix} D^{1111} & D^{1122} & D^{1133} & D^{1112} & D^{1123} & D^{1131} \\ D^{2211} & D^{2222} & D^{2233} & D^{2212} & D^{2223} & D^{2231} \\ D^{3311} & D^{3322} & D^{3333} & D^{3312} & D^{3323} & D^{3331} \\ D^{1211} & D^{1222} & D^{1233} & D^{1212} & D^{1223} & D^{1231} \\ D^{2311} & D^{2322} & D^{2333} & D^{2312} & D^{2323} & D^{2331} \\ D^{3111} & D^{3122} & D^{3133} & D^{3112} & D^{3123} & D^{3131} \end{bmatrix} \quad (17)$$

$$\bar{D}_b^a, \bar{D}_a^b \text{ y } \bar{D}_{ab}$$

In consequence \bar{D}_b^a , \bar{D}_a^b y \bar{D}_{ab} in matricial representation:

$$[\bar{D}_b^a] = \begin{bmatrix} D_{.,11}^{11} & D_{.,22}^{11} & D_{.,33}^{11} & | & 2D_{.,12}^{11} & 2D_{.,23}^{11} & 2D_{.,31}^{11} \\ D_{.,11}^{22} & D_{.,22}^{22} & D_{.,33}^{22} & | & 2D_{.,12}^{22} & 2D_{.,23}^{22} & 2D_{.,31}^{22} \\ D_{.,11}^{33} & D_{.,22}^{33} & D_{.,33}^{33} & | & 2D_{.,12}^{33} & 2D_{.,23}^{33} & 2D_{.,31}^{33} \\ D_{.,11}^{12} & D_{.,22}^{12} & D_{.,33}^{12} & | & 2D_{.,12}^{12} & 2D_{.,23}^{12} & 2D_{.,31}^{12} \\ D_{.,11}^{23} & D_{.,22}^{23} & D_{.,33}^{23} & | & 2D_{.,12}^{23} & 2D_{.,23}^{23} & 2D_{.,31}^{23} \\ D_{.,11}^{31} & D_{.,22}^{31} & D_{.,33}^{31} & | & 2D_{.,12}^{31} & 2D_{.,23}^{31} & 2D_{.,31}^{31} \end{bmatrix} \quad [\bar{D}_a^b] = \begin{bmatrix} D_{11}^{11} & D_{11}^{22} & D_{11}^{33} & | & D_{11}^{12} & D_{11}^{23} & D_{11}^{31} \\ D_{22}^{11} & D_{22}^{22} & D_{22}^{33} & | & D_{22}^{12} & D_{22}^{23} & D_{22}^{31} \\ D_{33}^{11} & D_{33}^{22} & D_{33}^{33} & | & D_{33}^{12} & D_{33}^{23} & D_{33}^{31} \\ 2D_{12}^{11} & 2D_{12}^{22} & 2D_{12}^{33} & | & 2D_{12}^{12} & 2D_{12}^{23} & 2D_{12}^{31} \\ 2D_{23}^{11} & 2D_{23}^{22} & 2D_{23}^{33} & | & 2D_{23}^{12} & 2D_{23}^{23} & 2D_{23}^{31} \\ 2D_{31}^{11} & 2D_{31}^{22} & 2D_{31}^{33} & | & 2D_{31}^{12} & 2D_{31}^{23} & 2D_{31}^{31} \end{bmatrix}$$

$$[\bar{D}_{ab}] = \begin{bmatrix} D_{1111} & D_{1122} & D_{1133} & | & 2D_{1112} & 2D_{1123} & 2D_{1131} \\ D_{2211} & D_{2222} & D_{2233} & | & 2D_{2212} & 2D_{2223} & 2D_{2231} \\ D_{3311} & D_{3322} & D_{3333} & | & 2D_{3312} & 2D_{3323} & 2D_{3331} \\ 2D_{1211} & 2D_{1222} & 2D_{1233} & | & 4D_{1212} & 4D_{1223} & 4D_{1231} \\ 2D_{2311} & 2D_{2322} & 2D_{2333} & | & 4D_{2312} & 4D_{2323} & 4D_{2331} \\ 2D_{3111} & 2D_{3122} & 2D_{3133} & | & 4D_{3112} & 4D_{3123} & 4D_{3131} \end{bmatrix} \quad (18)$$

Aplications and operations with numerical integration of constitutive equations

The stress and strain is contravariants y covariants components, for example:

$$\bar{s}^a = 2G\bar{I}^{dev,ab} : \bar{e}_b \quad (19)$$

For the elastic tensor in \mathbb{R}^6

$$\begin{aligned}\bar{D}^{ab} &= 3K\bar{I}^{vol,ab} + 2G\bar{I}^{dev,ab} \\ \bar{D}_{ab} &= 3K\bar{I}_{ab}^{vol} + 2G\bar{I}_{ab}^{dev} \\ \bar{D}_{.b}^a &= \bar{D}_a^{.b} = 3K\bar{I}_{.b}^{vol,a} + 2G\bar{I}_{.b}^{dev}\end{aligned}\quad (20)$$

Invariant principle in numerical integration

- Example 1:

$$\lambda = f(\sigma' : \varepsilon')$$

$$\lambda = f([\bar{\sigma}'^a]^T \cdot [\bar{\varepsilon}'^b])$$

- Example 2

$$\dot{\varepsilon}^p = \lambda \frac{\partial f}{\partial \sigma} \quad \text{will be} \quad \bar{\varepsilon}_b^p = \lambda \bar{I}_{ba} : \left(\frac{\partial \bar{f}}{\partial \sigma} \right)^a$$

- Example 3:

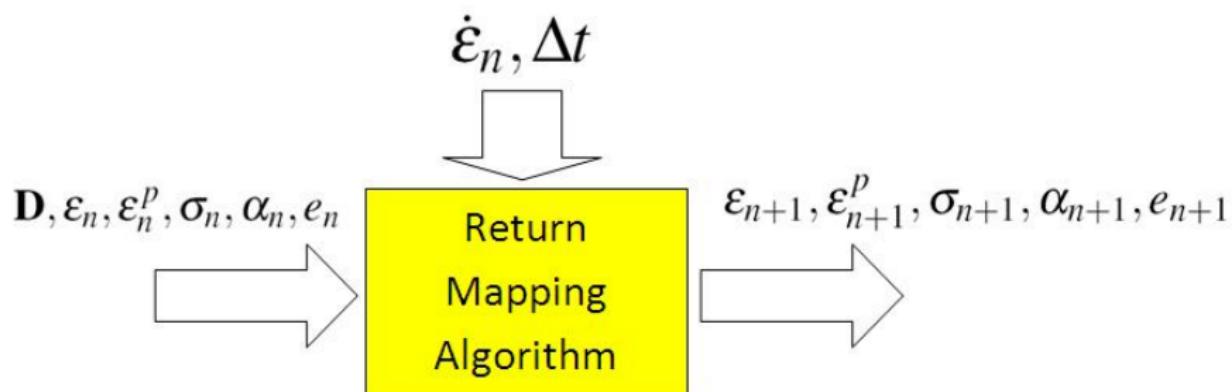
$$\dot{\sigma} = D : (\dot{\varepsilon} - \dot{\varepsilon}^p)$$

will be:

$$\bar{\sigma}^a = \bar{D}^{ab} : (\bar{\varepsilon}_b - \bar{\varepsilon}_b^p) \quad \text{or} \quad \bar{\sigma}^a = \bar{D}_{.b}^a : [\bar{I}^{bc} : (\bar{\varepsilon}_c - \bar{\varepsilon}_c^p)]$$

About of the numerical implementation

Return mapping algorithm



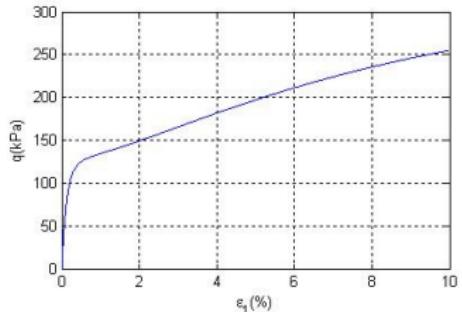
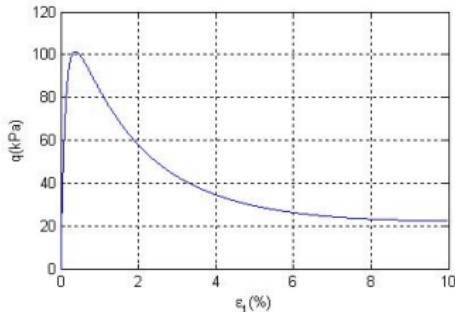
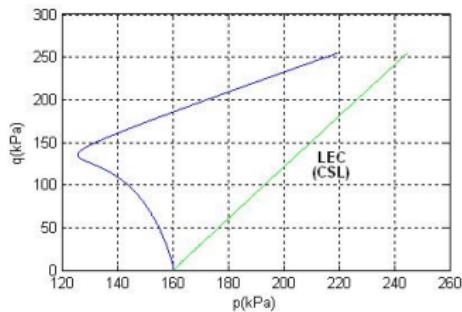
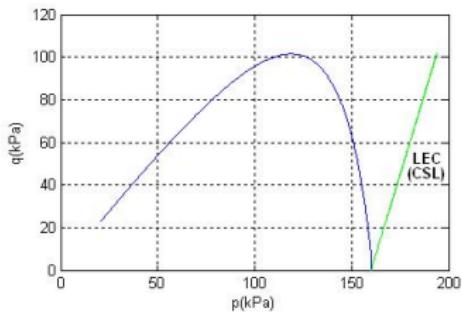
Model Constants, Nevada Sand

Simulations, Nevada Sand (Arulmoni et. al., 1992)

Elastic	G_0 K_0 a	3,14x10 ⁴ 3,14x10 ⁴ 0,6
Critical state	M_c λ $(e_c)_{ref}$	1,14 0,025 0,80
State Parameter	k_c^b k_c^d	3,975 4,20
Hardening	h_0 m	1200 0,05
Dilatancy	A	0,54

Results and Discussion

Toyura Sand - Dafalias (Sanisand, 2007)



- The results show that for the analyzed particular case, there is a saving on time until 15 % in \mathbb{R}^6 in relation to \mathbb{R}^3 . This is due to the smaller access to memory keeping and recovering data, as well as the diminution in the number of operations conducted by the transformation of \mathbb{R}^3 to \mathbb{R}^6 .
- The transformations done of the representation of tensors in \mathbb{R}^6 of covariants to contravariants and inversely, they can be easily made indicating the terms that are altered instead of making tensors multiplications with the identity tensors (covariants, contravariants or mixed), since these last multiplications are expensive in terms of computacional time.

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